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#### (54) Abstract Title

#### Mode shape converter having upper and lower optical rib waveguides

(57) A mode shape converter may be interposed between an input or output terminal of a function executing unit included in an optical device and an optical fibre. It serves to couple a mode of the optical fibre with a mode of the input or output terminal of the function executing unit. The mode shape converter includes a substrate 300, a lower cladding 302 coated over the substrate, a lower rib waveguide 304, a core 306 an upper rib waveguide 308 and upper cladding 310. The core and waveguides are made of a single medium. A stepped pattern defined by the lower rib waveguide exists partially only in the coupling 312 and conversion regions 314, thereby simplifying the pattern shape of the upper rib waveguide. Stabilisation region 316 is shown.

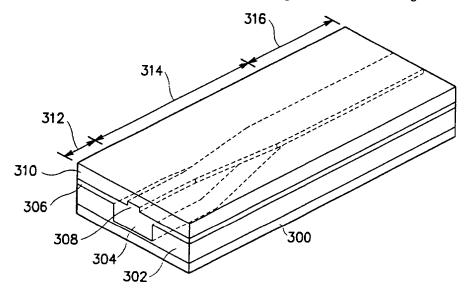


FIG.3

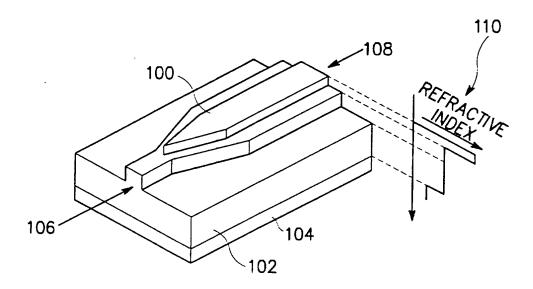
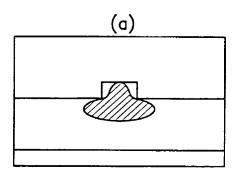


FIG.1



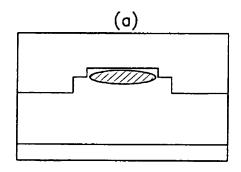


FIG.2

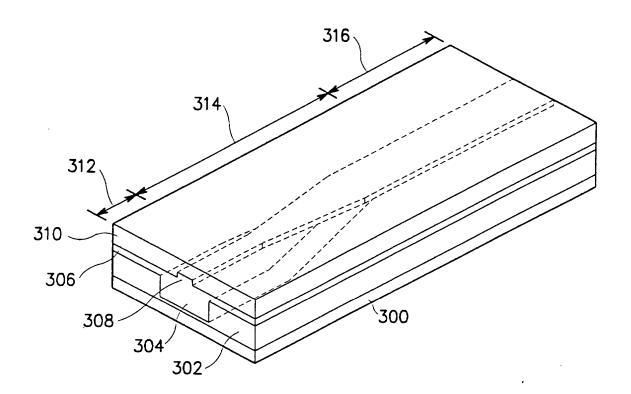


FIG.3

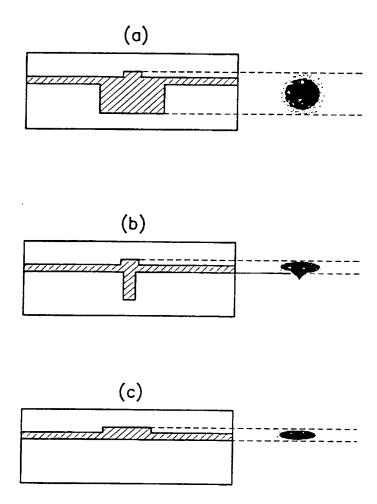


FIG.4

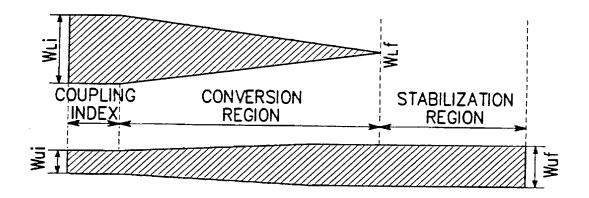


FIG.5

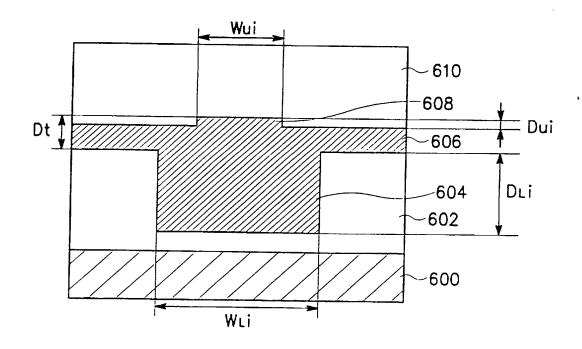


FIG.6

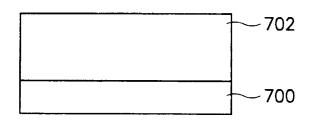


FIG.7A

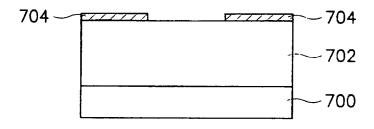


FIG.7B

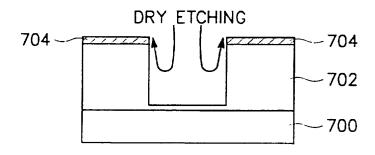


FIG.7C

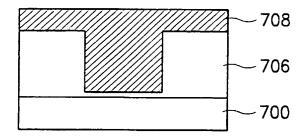


FIG.7D

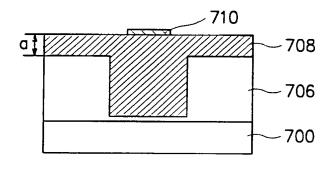


FIG.7E

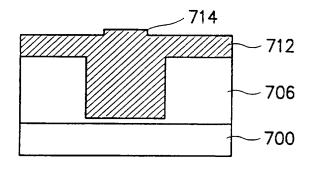


FIG.7F

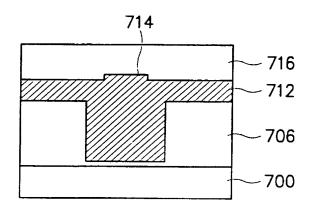
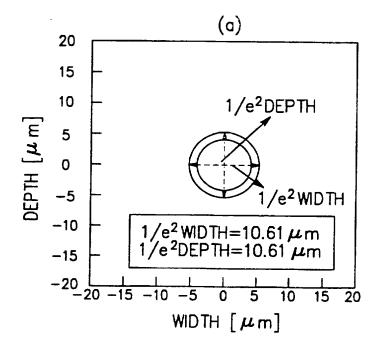


FIG.7G



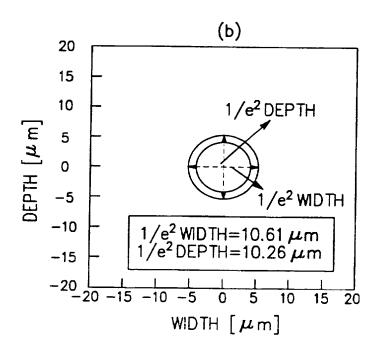


FIG.8

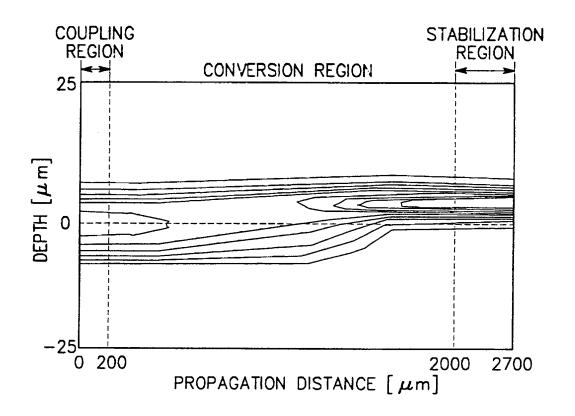


FIG.9

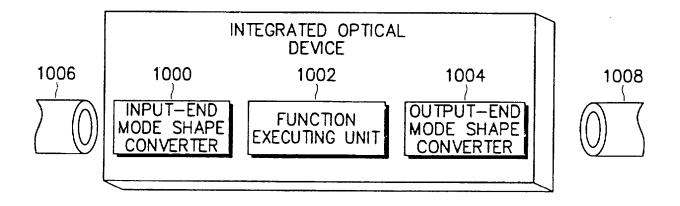


FIG.10

### MODE SHAPE CONVERTER FOR AN INTEGRATED OPTICAL DEVICE

The present invention relates to a mode shape converter, a method for fabricating the mode shape converter, and an integrated optical device using the mode shape converter. More particularly the invention concerns a mode shape converter arranged at an input or output terminal of an optical device and adapted to couple light inputted into or outputted from the optical device via optical fibres.

The present invention also relates to a method for fabricating such a mode shape converter, and an integrated optical device using the mode shape converter.

An integrated optical technique is a technique for integrating a variety of optical devices using waveguides on one substrate. Using such an integrated optical technique, it is possible to easily integrate an multifunctional optical device having a complicated structure on a limited small area because the alignment of unit optical devices can be easily made.

An example of a waveguide structure implementing an integrated optical device is a rib waveguide which is a channel waveguide fabricated by partially etching a planar waveguide. Such a rib waveguide has various advantages as follows. Firstly, it is possible to select respective refractive indices of a core and a cladding within a wide range. Secondly, it is possible to fabricate a single-mode waveguide having a large cross-sectional area irrespective of a refractive index difference between the core and cladding. Thirdly, it is

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possible to easily adjust optical characteristics such as a mode distribution and propagation constants under the condition in which an etched depth is used as a major process parameter. Fourthly, a precise pattern can be obtained, as compared to rectangular waveguides. because the etched depth in the rib waveguide is less than those of the rectangular waveguides. Fifthly, it is possible to reduce damages occurring during the etching process for a core layer, for example, errors in pattern size caused by an anisotropic etching, a cracking phenomenon occurring during the etching process for a layer having stresses, and damages caused by a accumulation of by-products formed during the etching process.

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In spite of such advantages, the above mentioned rib waveguide has the disadvantage that a very large coupling loss is generated when an optical fibre is coupled to the waveguide of the optical device. Single-mode optical fibres have a circular mode distribution having an aspect ratio of 1:1 while having a relatively large size, for example about 10  $\mu$ m. On the other hand, rib wavequides have an oval mode distribution in which the horizontal width is larger than the vertical width. In many cases, the mode distribution size of such a rib wavequide is also larger than those of the single mode optical fibres. For this reason, there is a misalignment in mode shape at the connection between a rib wavequide and an optical Due to such a mode shape misalignment, an optical wave encounters a discontinuity while passing through the connection, so there is a coupling loss due to reflection or scattering.

In order to solve this problem, a mode shape converter is arranged at the input or output terminal of the integrated optical device to which an optical fibre is coupled. The mode shape converter serves to convert slowly the mode of the optical fibre into a mode shape suitable for execution of the functions of the optical device, thereby achieving a reduction in coupling loss.

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A conventional mode shape converter is disclosed in U.S. Patent No. 5,078,516 and is illustrated in Figure 1 (see later). However, the mode shape converter of this patent has the disadvantage that it is difficult to manufacture precisely because the case is formed from two different materials. The mode shape converter also suffers from transmission loss.

It is an object of the invention is to provide a mode shape converter including a double waveguide made of a single medium having an up-tapering structure. It is an object of the invention that the core of the mode shape converter be made from the same material as the upper and lower rib waveguides. Manufacture of the mode shape converter should thus be achieved more easily and more accurately than prior art designs. It is also an aim to minimise coupling and transmission losses. The mode shape converter of the present invention achieves some or all of these aims.

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It is also an object to provide a method for fabricating

the mode shape converter, and an integrated optical device using the mode shape converter.

In accordance with one aspect, the present invention provides a mode shape converter adapted to couple a mode 5 of an optical fibre with a mode of the input or output terminal of a function executing unit, the mode shape lower cladding converter comprising: a substrate; a coated over the substrate, the lower cladding having an etched portion in a desired region; a lower rib waveguide 10 formed in the etched portion of the lower cladding; a core formed over both the lower rib waveguide and the non-etched portion of the lower cladding; an upper rib on the core and substantially formed wavequide alignment with the lower rib waveguide; and an upper 15 cladding formed over both the upper rib waveguide and a portion of the core not covered with the upper rib waveguide.

In accordance with another aspect, the present invention 20 provides a method for fabricating a mode shape converter lower cladding over a comprising: (a) coating patterning an etch mask on the lower substrate; (b) cladding, and etching the lower cladding to a desired depth using the resultant pattern of the etch mask; (c) 25 coating a core layer over the etched lower cladding, thereby forming a lower rib waveguide and a core; (d) patterning another etch mask on the core, and etching the core using the resultant pattern of another etch mask, thereby forming an upper rib waveguide; and (e) coating 30 upper cladding on the core and the upper

waveguide.

The mode shape converter of the present invention can be used in an integrated optical device. Such a device may include a function executing unit coupled to optical 5 and output terminals input fibres at respectively, a first mode shape converter arranged at the input terminal of the function executing unit and adapted to convert an input optical fibre mode into a mode suitable for execution of desired functions of the 10 optical device, and a second mode shape converter arranged at the output terminal of the function executing unit and adapted to convert a mode outputted from the function executing unit into an optical fibre mode, the second mode shape converter having an arrangement reverse 15 to that of the first mode shape converter, wherein each and second mode shape converters is the first separately formed in accordance with the invention.

20 The present invention will now be illustrated by way of example only with reference to the following drawings in which:

Fig. 1 is a perspective view illustrating the 25 structure of a conventional mode shape converter;

Fig. 2a is a diagram illustrating a mode profile of the input terminal in the mode shape converter shown in Fig. 1;

Fig. 2b is a diagram illustrating a mode profile of the output terminal in the mode shape converter shown in Fig. 1;

Fig. 3 is a perspective view illustrating the structure of a mode shape converter according to the present invention;

Figs. 4a, 4b and 4c are diagrams illustrating respective cross-sectional shapes of regions shown in Fig. 3 along with respective mode profiles in those regions;

Figs. 5a and 5b are plan views respectively illustrating lower and upper rib waveguides shown in Fig.

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Fig. 6 is a cross-sectional view illustrating a coupling region of the mode shape converter according to the present invention;

Figs. 7a to 7g are cross-sectional views respectively illustrating sequential processing steps of a method for fabricating the mode shape converter in accordance with the present invention;

Figs. 8a and 8b are diagrams respectively illustrating the mode of an optical fibre and the mode of a double rib waveguide according to the present invention:

Fig. 9 is a diagram of the results of a simulation conducted in accordance with a three-dimensional beam propagation method, illustrating the operation of a conversion region shown in Fig. 3; and

Fig. 10 is a schematic view illustrating an integrated optical device using mode shape converters having a configuration according to the present invention.

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The mode shape converter shown in Fig. 1 includes a first

waveguide 100, a second waveguide 102, and a substrate In Fig. 1, the reference numeral 106 denotes an input terminal whereas the reference numeral 108 denotes an output terminal. The reference numeral 110 represents respective refractive indices of the first waveguide 100, second waveguide 102, and substrate 104. The first waveguide 100 is designed to have a small mode size suitable for execution of the functions of an optical device to which the mode shape converter is coupled. second waveguide 102 is designed to have a refractive index less than that of the first waveguide 100 while having a large mode size to obtain an advantageous input/output coupling with an optical fibre. The input terminal 106 has a waveguide constituted only by the second waveguide 102. This second waveguide 102 uses air as its upper cladding while using the substrate 104 as its lower cladding in order to confine optical waves in a depth direction. In order to confine optical waves in a longitudinal direction, the second waveguide 102, which serves as a core, is partially etched to have a rib waveguide structure.

The output terminal 108 has a waveguide constituted only by the first waveguide 100. The first waveguide 100 of the output terminal 108 has a strip loaded waveguide structure different from the rib waveguide structure of the input terminal 106. The first waveguide 100 uses air as its upper cladding while using the second waveguide 102 as its lower cladding.

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A mode conversion region is defined between the input and

output terminals 106 and 108 in order to convert a mode coupled after being inputted from the optical fibre to the optical device into a mode shape suitable for execution of the functions of the optical device without any loss of the coupled mode. The rib waveguide having a large mode size is converted into the strip loaded waveguide having a small mode size by the mode conversion region. A light guided through the mode shape converter is slowly shifted toward the first waveguide 100 because the first waveguide 100 has a refractive index higher than that of the second waveguide 102 even though the widths of both the first and second waveguides 100 and 102 increase. When the guided light reaches the output terminal 108, the power thereof is mainly concentrated toward the first waveguide 100.

Fig. 2a is a diagram illustrating a mode profile of the input terminal 106 in the above mentioned mode shape converter whereas Fig. 2b is a diagram illustrating a mode profile of the output terminal 108 in the mode shape converter.

However, the integrated optical device provided with the above mentioned mode shape converter of the prior art has problems as follows. First, the fabrication is troublesome because it is necessary to use two cores made of different materials, and the first waveguide should be precisely formed on the second waveguide. Second, there is a limitation in minimizing the coupling loss of the optical device to an optical fibre having a circular mode because the input terminal 106 has a rib waveguide

structure having an oval waveguide mode even though it has a large mode size. Third, since the mode shape converter uses a down-tapering structure in order to increase the mode size of the input-end waveguide, its waveguide taper increases in length. An increase in transmission loss occurs during the mode conversion.

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Fig. 3 is a perspective view illustrating the structure of a mode shape converter according to the present invention. The mode shape converter of Fig. 3 includes a substrate 300, a lower cladding 302, a lower rib waveguide 304, a core 306, an upper rib waveguide 308, and an upper cladding 310. In Fig. 3, the reference numeral 312 denotes a coupling region, 314 a conversion region, and 316 a stabilization region. The lower rib waveguide 304, core 306, and upper rib waveguide 308 are made of the same material.

Figs. 4a, 4b and 4c are diagrams illustrating respective cross-sectional shapes of the coupling region 20 conversion region 314, and stabilization region 316 shown in Fig. 3 along with respective mode profiles in those regions. Referring to Figs. 4a to 4c, it can be seen the circular mode of the coupling region 25 connected to an optical fibre is gradually converted into an oval shape while passing though the conversion region 314. After passing though the stabilization region 316, the mode is converted into an oval mode suitable for execution of the functions of an optical device to which 30 the mode shape converter is applied.

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Figs. 5a and 5b are plan views respectively illustrating the lower rib waveguide 304 and upper rib waveguide 308 shown in Fig. 3. In Figs. 5a and 5b, " $W_{t,i}$ " and " $W_{t,i}$ " represent respective input-end widths of the lower and upper rib waveguides whereas "W,, and "W,, represent respective output-end widths of the lower and upper rib Referring to Figs. 5a and 5b, it can be wavequides. found that each waveguide has a structure varying That is, the lower accordance with each region thereof. rib waveguide 304 has a width decreasing gradually to 0 has the upper rib waveguide 308 a whereas increasing gradually to a width suitable for execution of the functions of the optical device. Herein, device include modulation, functions of the optical switching or filtering of optical waves. The coupling 15 region 312 is a region where the mode shape converter is coupled to an optical fibre. This coupling region 312 is designed to have a mode having the same size and shape as those of the mode of the optical fibre. This coupling region has a double rib waveguide structure having a core 20 This double rib waveguide made of a single medium. structure includes two waveguides one being the upper rib waveguide 308 while the other waveguide being the lower 304 arranged beneath the upper rib rib waveguide waveguide 308 in an inverted state. The upper rib 25 waveguide 308 is connected to a function executing unit of the optical device. The lower rib waveguide 304 has a width and a depth adjusted to allow the fundamental mode of the double rib waveguide to well coincide with the circular mode of the optical fibre. 30

The conversion region is a region in which optical waves coupled in the coupling region 312 are converted into a mode shape suitable for execution of the functions of the This conversion region is designed to optical device. satisfy adiabatic conditions in order to minimize the radiation loss generated during the conversion. conversion region, the lower rib waveguide 304 decreases gradually in width as it extends longitudinally, thereby causing the circular mode of the coupling region to be converted into an oval rib waveguide mode suitable for execution of the functions of the optical device. As the width of the lower rib wavequide 304 decreases gradually, the power of light waves confined in the lower waveguide 304 decreases gradually. As a result, the light waves migrate to the upper rib waveguide 308.

Respective width variations of the lower and upper rib waveguides 304 and 308 are designed to minimize the radiation loss.

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The stabilization region 316 serves to remove higherorder modes generated during the mode conversion, thereby mode suitable for execution of transmitting а functions of the optical device to the function executing unit of the optical device. This stabilization region 316 is constituted only by the upper rib waveguide 308. The stabilization region 316 allows only the mode of the converted optical waves suitable for execution of desired functions while radiating the remaining higher-order modes to the substrate.

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mode shape converter having the above mentioned structure is fabricated in accordance with the following design. The present invention takes into consideration a rib waveguide having an oval mode shape. The structure input-end waveguide is then determined which coincides with the mode shape of the optical fibre. Where the area of the input-end waveguide is reduced to make the mode shape of the waveguide coincide with the mode shape of the optical fibre, as in the down-tapering method, it is difficult to achieve an efficient input coupling even when a small variation in the crossshape of optical waveguide sectional the occurs. Accordingly, a waveguide structure having a large crosssectional area is designed, as in the up-tapering method, in order to achieve an efficient input coupling and to increase an error tolerance of the waveguide crossaccordance with the present shape. In sectional invention, a double rib waveguide structure is fabricated single rib waveguide (upper includes a which waveguide), and an inverted rib waveguide (lower rib waveguide) arranged beneath the upper rib waveguide while having a large cross-sectional area, so that it has a mode having a large mode size and a circular mode shape.

Thereafter, a waveguide taper is designed which connects the input and output terminals. In order to convert a large circular mode into an oval mode, it is necessary to form a taper extending in a depth direction. In accordance with the present invention, the lower and upper rib waveguides 304 and 308 are designed in such a fashion that the tapering effect in the depth direction

is obtained even though only a tapering in a width direction is made. When the width of the lower rib waveguide 304 is gradually reduced, the optical waves traveling along the lower rib waveguide 304 migrate gradually in an upward direction to the upper rib waveguide 308. Respective width variations of the upper and lower rib waveguides 308 and 304 are determined to minimize the radiation loss generated during the mode conversion.

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design for the cross section of the mode Fig. 6 is a crossconverter is conducted as follows. sectional view illustrating the coupling region of a mode shape converter according to the present invention. Fig. 6, the reference numeral 600 denotes a substrate, 602 a lower cladding, 604 a lower rib waveguide, 606 a core, 608 an upper rib waveguide, and 610 an upper "W<sub>iii</sub>" represents the input-end width of the cladding. upper rib waveguide 608, "D," the thickness of the core 606, "D<sub>m</sub>" the etched depth for formation of the upper rib waveguide 608, " $D_{Li}$ " the etched depth for formation of the lower rib waveguide 604, and " $W_{Li}$ " the input-end width of the lower rib waveguide 604. These parameters can be determined as follows. For example, where the upper rib waveguide is designed to have a structure suitable for execution of the functions of the optical device by determining the parameters  $D_r$ ,  $D_{ts}$ , and  $W_{ts}$ , the remaining parameters  $W_{Li}$ ,  $D_{Li}$ , and  $W_{Ui}$  can be determined using the following Expression 1. The coupling efficiency can be derived by an overlap integral of the mode of the double rib waveguide with the mode of the optical fibre.

overlap integral is expressed by the following Expression 1 in accordance with a coupled mode theory.

#### [Expression 1]

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$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} E_{Coupling \ Re \ gion}(x,y) \cdot E_{Coupling \ Re \ gion}(x,y) ds \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} E_{Optical \ Fiber}(x,y) \cdot E_{Optical \ Fiber}(x,y) ds$$

where,  $E_{\text{Optical Fibre}}$  and  $E_{\text{Coupling Region}}$  represent respective mode distributions of the optical fibre and coupling region.

In accordance with the above Expression 1, when the above two mode distributions are identical to each other and accurately aligned with each other, the overlap integral value is 1. A mode shape converter is fabricated using the patterns and etched depths of the lower and upper rib waveguides fabricated in accordance with the above mentioned design. Figs. 7a to 7g illustrate a method for fabricating the above mentioned mode shape converter in accordance with the present invention. For the material of the mode shape converter, a semiconductor material such as Si, GaAs or InP, a dielectric material such as LiNbO<sub>3</sub>, or a polymer may be used.

The method illustrated in Figs. 7a to 7g corresponds to the case in which a polymer is used to fabricate the mode shape converter. In accordance with this method, a polymer is first coated over a silicon substrate 700, thereby forming a lower cladding 702, as shown in Fig. 7a. An etch mask pattern 704 is then formed on the lower cladding 702 in accordance with a photolithography using a dark field mask in order to form a lower rib waveguide,

as shown in Fig. 7b. The lower cladding 702 is then dryetched to a desired depth using the etch mask pattern 704, as shown in Fig. 7c. Thereafter, a polymer is etched lower cladding coated over the 706, thereby forming a core 708, as shown in Fig. 7d. In order to form an upper rib waveguide, a bright field mask is then aligned with the lower rib waveguide. Using the bright an etch mask pattern 710 is formed field mask, accordance with photolithography, as shown in Fig. 7e. Using the etch mask pattern 710, the core 708 is then dry-etched to a depth determined in the above procedure, thereby forming a core 712 and an upper rib waveguide 714, as shown in Fig. 7f. A polymer is then coated over the core 712 and upper rib waveguide 714, thereby forming an upper cladding 716, as shown in Fig. 7g.

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Figs. 8a and 8b illustrates the mode of the optical fibre and the mode of the double rib waveguide according to the present invention, respectively. In order to determine the degree of the coupling between the optical fibre and the double rib waveguide, the coupling efficiency of the mode shape converter was calculated in accordance with a analysis method using a section mode difference method while using the above mentioned overlap integral Expression in accordance with the In the case of the optical fibre mode shown in Fig. 8a, the core and cladding of the optical fibre have refractive indices of 1.461 and 1.457 (specific refractive index  $\Delta n = 0.27 \%$ ). The core of the optical fibre has a diameter of 9  $\mu$ m. The mode of the optical fibre is a circular mode in that both the 1/e2 width and  $1/e^2$  depth of the intensity of optical waves are 10.61  $\mu m$  at a wavelength of 1.55  $\mu m$ .

The parameters of the double rib waveguide used in the numeric simulation are as follows. Respective refractive 5 indices of the core and cladding are 1.5337 and 1.5169 (specific refractive index  $\Delta n = 1.2 \%$ ). The width of the upper rib waveguide,  $W_{\text{uf}},$  is 5  $\mu m,$  the etched depth  $D_{\text{ui}}$  is 1.5  $\mu$ m, and the thickness of the core,  $D_t$ , is 4.0  $\mu$ m. width  $W_{\text{Li}}$  and etched depth  $D_{\text{Li}}$  of the lower rib waveguide 10 exhibiting a maximum coupling efficiency are derived by conducting a calculation for the coupling efficiency while varying the width and depth of the lower rib waveguide. When "W $_{\rm Li}$ " is 11.5  $\mu m$ , and "D $_{\rm Li}$ " is 7.5  $\mu m$ , a maximum integral value of 0.9889 is obtained. This value 15 corresponds to a coupling loss of 0.05 dB which is a small coupling loss. In this case, the mode of the coupling region exhibits a  $1/e^2$  width and a  $1/e^2$  depth of the intensity of optical waves respectively corresponding to 10.61  $\mu m$  and 10.26  $\mu m$ , and an aspect ratio of 1.034. 20

The conversion region is a region for varying respective widths of the lower and upper rib waveguides in order to transmit, to the rib waveguide of the stabilization region, the optical waves coupled after being inputted to the coupling region. The width of the upper rib waveguide varies from the input-end width  $W_{0i}$  of the mode shape converter to the output-end width  $W_{0i}$  at the output terminal of the mode shape converter connected to the optical device. The width of the lower rib waveguide decreases gradually to 0 in a longitudinal direction. As

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a result, the conversion region serves to migrate the optical waves from the lower rib waveguide to the upper rib waveguide.

5 Fig. 9 is a diagram of the results of a simulation conducted in accordance with a three-dimensional beam propagation method, illustrating the operation of the conversion region. In Fig. 9, the dark portion represents regions where a high intensity of light is exhibited.

Referring to Fig. 9, it can be found that the optical waves confined in the lower rib waveguide in the coupling region migrate gradually toward the upper rib waveguide while passing through the conversion region. The optical waves migrated to the upper rib waveguide radiate higher-order modes while passing through the stabilization region. After radiating the higher-order modes, the optical waves are transmitted to the optical device.

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Fig. 10 is a schematic view illustrating an integrated optical device using mode shape converters having a configuration according to the present invention. As shown in Fig. 10, the integrated optical device includes an input-end mode shape converter 1000, a function executing unit 1002, and an output-end mode shape converter 1004 having an arrangement reverse to that of the input-end mode shape converter 1000.

The input and output-end mode shape converters 1000 and 1004 are connected to optical fibres 1006 and 1008,

respectively. The input-end mode shape converter 1000 converts the mode of an optical wave received from the optical fibre 1006, and then outputs the converted mode to the function executing unit 1002. The output-end mode shape converter 1004 converts the mode outputted from the function executing unit 1002 into a circular mode which is, in turn, outputted to the second optical fibre 1008. Therefore, the output-end mode shape converter 1004 has an arrangement reverse to that of the input-end mode shape converter 1000 in the integrated optical device.

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As is apparent from the above description, the core used to fabricate the mode shape converter according to the present invention is made of a single medium. mode shape converter of the present invention, stepped pattern defined by the lower rib waveguide exists partially only in the coupling and conversion regions, thereby simplifying the pattern shape of the upper rib Accordingly, the fabrication of the mode waveguide. shape converter is simplified. The mode shape converter coupling the present invention provides a hiqh efficiency because the input-end waveguide thereof has a circular mode. Since an up-tapering structure adapted to gradually increase the waveguide width is used for the input-end waveguide, it is possible to reduce the taper length of the waveguide while reducing the transmission loss during the mode conversion.

#### Claims

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- 1. A mode shape converter adapted to couple a mode of an optical fibre with a mode of the input or output terminal of a function executing unit, the mode shape converter comprising:
  - a substrate;
- a lower cladding coated over the substrate, the lower cladding having an etched portion in a desired region;
  - a lower rib waveguide formed in the etched portion of the lower cladding;
  - a core formed over both the lower rib waveguide and the non-etched portion of the lower cladding;
- an upper rib waveguide formed on the core and substantially in alignment with the lower rib waveguide; and
- an upper cladding formed over both the upper rib waveguide and a portion of the core not covered with the upper rib waveguide.
  - 2. A mode shape converter as claimed in claim 1, wherein the lower rib waveguide comprises:
- a coupling region having a mode coupled with the 25 mode of the optical fibre; and
  - a conversion region having a width decreasing gradually from the width of the coupling region to 0 in such a fashion that it transmits the mode of the coupling region to the upper rib waveguide.

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3. A mode shape converter as claimed in claim 2, wherein

the width of the coupling region decreases gradually so that a radiation loss generated during the transmission of the mode from the coupling region to the upper rib waveguide is minimized.

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- 4. A mode shape converter according to claim 2, wherein the coupling region has, at an input end thereof, a cross section having a width and a thickness determined based on the thickness of the upper rib waveguide and the output-end width of the upper rib waveguide in such a fashion that a coupling efficiency between the mode of the optical fibre and the mode of the coupling region is maximized.
- 15 5. A mode shape converter as claimed in any preceding claim, wherein the upper rib waveguide comprises:
  - a coupling region aligned with the coupling region of the lower rib waveguide;
- a conversion region aligned with the conversion region of the lower rib waveguide and adapted to convert the mode transmitted from the lower rib waveguide into a mode suitable for the function executing unit; and
- a stabilization region for outputting the mode transmitted from the conversion region to the function executing unit.
  - 6. A mode shape converter as claimed in any preceding claim, wherein the coupling region of the upper rib waveguide has an input-end width determined based on the thickness of the core, the thickness of the upper rib waveguide and the output-end width of the upper

rib waveguide in such a fashion that the coupling efficiency between the mode of the optical fibre and the mode of the coupling region in the lower rib waveguide is maximized.

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- 7. A mode shape converter as claimed in claim 6, wherein the width of the coupling region in the upper rib waveguide varies so that a radiation loss generated during the conversion of the mode from the coupling region into the mode suitable for the function executing unit is minimized.
- 8. A mode shape converter as claimed in any preceding claim, wherein the upper rib waveguide, the core, and the lower rib waveguide are made of the same material.
  - 9. A mode shape converter as claimed in any preceding claim, wherein the dimensions of the mode shape converter are determined so as to maximise the value of the following formula:

$$\int_{-\infty}^{\infty} E_{Coupling \ Re \ gion}(x,y) \cdot E_{Coupling \ Re \ gion}(x,y) ds \int_{-\infty}^{\infty} E_{Optical \ Fiber}(x,y) \cdot E_{Optical \ Fiber}(x,y) ds$$

where  $E_{\text{optical}}$   $_{\text{Fibre}}$  and  $E_{\text{coupling}}$   $_{\text{Region}}$  respective mode distributors of the optical fibre and coupling region.

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- 10. A method for fabricating a mode shape converter comprising:
  - (a) coating a lower cladding over a substrate;
- (b) patterning an etch mask on the lower cladding, 30 and etching the lower cladding to a desired depth using the resultant pattern of the etch mask;

- (c) coating a core layer over the etched lower cladding, thereby forming a lower rib waveguide and a core;
- (d) patterning another etch mask on the core, and etching the core using the resultant pattern of another etch mask, thereby forming an upper rib waveguide; and

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- (e) coating an upper cladding on the core and the upper rib waveguide.
- 10 11. A method as claimed in claim 10, wherein the patterns respectively formed at the steps (b) and (c) are determined based on parameters determined to maximize a coupling efficiency between the input-end mode of the mode shape converter and the mode of the optical fibre.
  - 12. A method according to claim 11, wherein the width of each of the patterns varies so that a radiation loss generated during a conversion of the input-end mode of the mode shape converter into a mode suitable for an operation of the function executing unit is minimized.
- 13. A method as claimed in claim 12 wherein minimisation of the valuation loss is calculated by maximising the value of the following formula:

$$\int_{-\infty}^{\infty} E_{Coupling \ Re \ gion}(x,y) \cdot E_{Coupling \ Re \ gion}(x,y) ds \int_{-\infty}^{\infty} E_{Optical \ Fiber}(x,y) \cdot E_{Optical \ Fiber}(x,y) ds$$

where E optical fibre and E coupling region represent respective mode distributors of the optical

fibre and coupling region.

- An integrated optical device including a function executing unit coupled to optical fibres at input and output terminals thereof, respectively, a first 5 mode shape converter arranged at the input terminal function executing unit and adapted to of the convert an input optical fibre mode into a mode suitable for execution of desired functions of the optical device, and a second mode shape converter 10 arranged at the output terminal of the function adapted to convert a mode executing unit and outputted from the function executing unit into an optical fibre mode, the second mode shape converter having an arrangement reverse to that of the first 15 mode shape converter, wherein each of the first and second mode shape converters is separately defined by any of claims 1 to 9 or 15.
- 20 15. A mode shape converter substantially as hereinbefore described with reference to Figures 3 to 10 of the accompanying drawings.
- 16. A method substantially as hereinbefore described 25 with reference to Figures 3 to 10 of the accompanying drawings.







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Claims searched: 1-16 **Examiner:** 

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## Patents Act 1977 Search Report under Section 17

#### **Databases searched:**

UK Patent Office collections, including GB, EP, WO & US patent specifications, in:

UK Cl (Ed.R): G2J(JGDA, JGDBF, JGFX)

Int Cl (Ed.7): G02B

Other: Online: WPI, EPODOC, JAPIO

#### Documents considered to be relevant:

Category	Identity of document and relevant passage	Relevant to claims
A	GB 2317023 A (BOOKHAM) Fig 1	
n	Optics Letters, Vol 16, No 5, 1 March 1991, pp 306-8 R N Thurston et al	

Document indicating lack of novelty or inventive step Document indicating lack of inventive step if combined with

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